Interaction of large scale flow structures with gyrokinetic turbulence

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Shear flows have a profound influence on turbulence-driven transport in tokamaks. The introduction of arbitrary initial flow profiles into the code ORB5 (Jolliet et al., Comput. Phys. Commun. 177, 409 (2007)) allows the convenient study of how flows on all length scales both influence transport levels and self-consistently evolve. A formulation is presented which preserves the canonical structure of the background particle distribution when either toroidal or poloidal flows are introduced. Turbulence suppression is possible above a certain shearing rate magnitude for homogeneous shear flows, and little evolution of the shearing rate is seen. However, when a flow with a zone boundary, where the shearing rate reverses at mid-radius, is introduced, the shear flow evolves substantially during the simulation. \( E \times B \) shear flows with a zone boundary of a positive sign decay to a saturation amplitude, consistent with the well known saturation of turbulently generated zonal flows. Unlike the \( E \times B \) flow, the parallel flows relax diffusively. © 2011 American Institute of Physics.

I. INTRODUCTION

Gyrokinetic turbulence modelling indicates that the self-consistent flows driven by drift wave turbulence can substantially suppress transport levels in tokamaks. Imposing a homogeneous background (toroidal or poloidal), flow shear can reduce transport levels even further. However, the physics of turbulence-scale and global-scale flows have been investigated as separate topics. A comprehensive understanding of the physics of the interaction between shear flows on the full range of length scales and turbulence is lacking.

For example, the process which limits the amplitude of self-consistently driven shear flows has not been seen to act on homogeneous flow shears applied as an initial condition. We would like to know what suppresses this saturation mechanism for large-scale flows. Understanding this is particularly crucial for the physics of transport barriers, where flow structures form on intermediate length scales.

We study this problem numerically using the global gyrokinetic code ORB5 (Ref. 1). In order to systematically investigate both homogeneous shear flows and the zig-zag type flows seen in quasi-steady state gyrokinetic simulations, we allow arbitrary flow profiles as an initial condition in the code. This requires a definition of the background gyrocentre distribution \( f_0 \) which allows poloidal and toroidal flows with arbitrary profile. In order that \( f_0 \) remains a canonical distribution (i.e., constant along trajectories when the perturbed electric field is zero), the background electrical potential enters into the definition of the distribution function.

We then perform a series of numerical tests to examine how the structure of the background shear flow modifies turbulence levels and to examine the dynamics of the flow structures. First, the effect of a homogeneously sheared background flow is examined, partly as a benchmark against previous simulations. Second, we examine the linear and nonlinear evolution for “V-shaped” flow profiles where the sign of the flow shearing rate changes at mid radius. The zone boundaries, where the sign of the flow shearing rate changes, are shown to play a critical role in self-consistently limiting the shearing-rate.

II. GLOBAL GYROKINETIC EQUILIBRIA WITH BACKGROUND SHEAR FLOW

We consider small background flows, with \( v_e/v_{th} \ll 1 \), so that we ignore the transonic terms that arise when the \( E \times B \) flows are of order 1. Note however that we expect to largely recover the effects of the Coriolis and centrifugal forces for toroidally rotating plasmas, which are mostly associated with strong flow along the magnetic field. In this limit, the standard gyrokinetic formulism is valid, and we simply start from a different initial condition for the flow and electric field. To consider plasmas with a background electric potential \( \phi_0 \), we consistently modify the background distribution \( f_0 \) and substitute \( \phi \rightarrow \phi_0 + \phi \) in the zeroth order gyrokinetic equations of motion. We also introduce parallel flows in \( f_0 \) such that the sum of the \( E \times B \) and parallel flows is either dominantly poloidal or dominantly toroidal. The Vlasov-Poisson equations are unmodified, but the equations for \( \delta \phi \) are modified due to the different \( f_0 \). In principle, we could add an initial flow in the initial perturbation \( \delta f_0 \), but incorporating the flow perturbation in \( f_0 \) means that \( \delta \phi \) and, therefore, noise can be reduced, and linear dynamics can be conveniently treated.

Here, we require that the background distribution function be a collisionless gyrokinetic equilibrium, so that \( f_0 \) is constant along the unperturbed gyrocentre orbits. If the background equilibrium is chosen to be a local Maxwellian, as in some gyrokinetic codes, one must either tolerate large transient fluxes at the beginning of the simulation or ignore terms...
arising from the derivatives of \( f_0 \) along the gyrocentre trajectory.

In order for \( f_0 \) to be a collisionless equilibrium, \( f_0 \) must only be a function of the three canonical momenta: the energy \( \epsilon = m v^2 / 2 + q \phi_0 \), toroidal canonical momentum \( \psi_c = \psi(\mathbf{R}) + m v_{R||} B_{\perp} / q B \), and magnetic moment \( \mu \). We suppress the gyroaveraging for the background field \( \phi_0 \), which will vary on scales considerably longer than the gyroradius. We define a canonical Maxwellian

\[
f_0 = \frac{n_0(Y)}{(2 \pi T(Y)/m)^{3/2}} \exp \left(-\frac{\epsilon - q \phi_0(\psi)}{T(Y)}\right),
\]

where \( \psi_c(\psi, \epsilon, \mu) \) is a modified canonical momentum which will be chosen later and \( Y \) is the “corrected” canonical momentum defined in Ref. \( 3 \). The toroidal canonical momentum is equal to the poloidal flux at zeroth order in \( \rho^* \), and thus can be used as a radial parameter; in the \( \rho^* \rightarrow 0 \) limit, this equilibrium is locally Maxwellian, with temperature and density varying as a function of radius. To make the dependence on \( \phi_0 \) more explicit, the exponent in the definition of \( f_0 \) can be written \( (m v^2/2 + q \phi_0(\psi) - q \phi_0(\psi_c)/T) \). The addition of the \( q \phi_0(\psi_c) \) term is necessary in order that \( \int d\psi f_0 \approx n_0 \), so that the density and the electric potential can be independently specified.

The initial electron density is assumed to almost neutralise the initial ion density, to give the prescribed initial electric field. In practice, we do not calculate the \( n_e \), exactly, but instead, the approximation \( n_e(\psi) \approx n_0(\psi_c) \approx f_0 \) is used for the electron density which appears in the quasineutrality approximation, neglecting terms of order \( \rho^* \).

The equations of motion are as before, except with an \( E \times B \) flow incorporated into the equations of motion

\[
\frac{dR}{dt} = \frac{v_{\parallel}}{B_{\parallel}} \mathbf{B}^* + \frac{v_{\perp}^2}{2 \Omega_e B_{\parallel}} \mathbf{B} \times \nabla B + \frac{(E_0 + \langle E_\parallel \rangle) \times \mathbf{B}}{B^* B_{\parallel}};
\]

and

\[
\frac{dv_\parallel}{dt} = \frac{\mathbf{B}^*}{m B_{\parallel}} \left(-\frac{m e v^2}{2B} \nabla B + q_i \nabla (\phi_0 + \langle \phi_i \rangle)\right).
\]

The evolution equation for \( \delta f = f(R, t) - f(R, t_0) \) is then

\[
\frac{d\delta f}{dt} = -f_0 \kappa(Y) \frac{dY}{dt} + \frac{q_0}{T_i(Y)} \langle E \rangle \frac{dR}{dt} \bigg|_{t_0} - f_0 q \frac{d\phi_0(\psi_c)}{d\psi_c} \frac{d\psi_c}{dt},
\]

with

\[
\kappa(Y) = \frac{n_0(Y)}{n_0(\psi_c)} \frac{3 T_i(Y)}{2 T_i(Y)} + \left(1 - q \phi_0(\psi_c)/T(Y)\right) T_i(Y) \frac{dY}{d\psi_c}.
\]

The \( \phi_0 d\psi_c / dY \) term arises as before from the density and temperature gradients, and the second term results from the modification to the gyroenergy as the particles interact with the perturbed electric field. The third term arises directly from the inclusion of \( \phi_0 \) in the definition of \( f_0 \). Note that all three terms are modified due to the modified marker trajectories.

Choosing \( \psi = \psi_c \), the canonical toroidal momentum results in the a near “pure toroidal flow” case, with small poloidal flows arising from temperature and density gradients. The poloidal component of the parallel flow along the field line cancels the poloidal flow due to the \( E_0 \times B \) motion. Parallel flow appears because \( \psi - \psi_c \) is proportional to the parallel velocity, and \( \phi_0(\psi_c) - \phi_0(\psi) \propto E_i v_i \); the distribution (ignoring for a moment the density and temperature gradients) is simply a shifted Maxwellian in the small \( E_i \) limit. Because collisions are thought to keep the distribution quite close to neoclassical equilibrium for most fusion relevant parameters, it is desirable that our background equilibrium be close to neoclassical equilibrium. For \( \psi = \psi_c \), the solution is an exact neoclassical equilibrium for the case where there is zero temperature gradient and \( \partial \phi_0 / \partial \psi \) constant (with only ion-ion collisions); once temperature gradient is introduced, the departure from neoclassical equilibrium is small, of order \( \rho^* \).

On the other hand, choosing

\[
\psi = \psi_c = \psi(\mathbf{R}) + F v_{\parallel}/B - F(\mathbf{v}_{\parallel}/B),
\]

which we call the modified canonical toroidal momentum, results in a state with small parallel flows. Here, the angle brackets denote a bounce average along zeroth order trajectories. \( \psi_c \) is equal to the bounce average of \( \psi \), so that is can be considered a good “average radial position” variable. This choice minimises the distortion to the distribution function \( f_0 \) due to \( \phi_0 \), by reducing the RMS magnitude of the term \( \psi(\phi) - \psi_0(\psi_c) \). However, once the electrical potential difference across a banana orbit \( q E_i \rho / \alpha R \) becomes comparable to the thermal energy, \( f_0 \) departs strongly from Maxwellian: collisionless equilibria with poloidal flows are inherently far from local Maxwellian. For large enough flows, the distribution function becomes double-peaked, due to structures at the trapped-passing boundary, and may well be unstable to bump-on-tail instabilities (which would not be correctly modelled in the gyrokinetic ordering and on the spatial scales resolved). In practice, with \( q \sim 2 \) and \( \rho / \alpha \sim 3 \), this leads to a restriction to poloidal flows \( \lesssim 0.1 v_{th} \), because we have assumed that the distribution function is near-Maxwellian in our derivation of the gyrokinetic equations, and simulations with larger flows manifest flow-driven instabilities which we would not expect to correctly resolve. It is interesting that there may be a mechanism limiting the size of poloidal flows even in strictly collisionless toroidal devices.

Plasma flows driven by the flux-surface averaged component of the electrical potential are capable of secularly tilting turbulent structures superimposed on the flow. The main impact of these sheared flows can be captured by an effective shearing rate,

\[
\omega_{E \times B} = \frac{1}{q B} \frac{d}{dr} \left(\frac{q d\phi_0}{r} \right),
\]

which gives the rate at which turbulent structures will be sheared in the poloidal plane, once an overall toroidal propagation has been factored out.

To substantially stabilise drift wave turbulence with shear flows, the effective shearing rate would have to be
similar to typical growth rates. For a homogeneous flow shear with effective shearing rate of the order of (for example) the typical ion temperature gradient (ITG) growth rate $0.1c_\text{i}/a$, over the whole minor radius, we would have $E \times B$ shear flows $\sim 0.1v_{th}$ at the plasma edge. Poloidal flows of this size would usually violate the assumption that $f_0$ be close to Maxwellian. Toroidal flows would need to be $\sim v_{th}$, for typical $q \sim 2$ and $R/a \sim 3$, too large to be correctly modelled without adding transonic terms into our gyrokinetic model, and much larger than seen in typical measurements in the cores of tokamaks. For standard parameter choices, it is only possible to introduce large enough flow shear to substantially modify the turbulence, within the limits of our ordering, by restricting the region with strong shear flow to an interval of the minor radius; for example, in a localised internal transport barrier.

The local density and mean kinetic energy are not substantially modified by the imposition of a background electric field, for moderate values of the electric field strength, so substantial modifications are needed to the specified drift field, for moderate values of the electric field strength, so substantially modified by the imposition of a background electric field. Also, we have implicitly assumed that the electron density and background potential are flux surface functions, which would be inconsistent if the ion density varied with poloidal angle.

### III. SIMULATIONS WITH UNIFORM SHEAR FLOWS

A series of simulation scans with two different plasma configurations were performed, with homogeneously sheared toroidal and poloidal flows. The STD case used in Ref. 4, which also investigated stabilisation with shear flow, serves as a convenient choice for benchmarking. For this case, $q = 2$, $(r/q)dq/dr = 1.0$, $R/L_T = 9$ at midradius, and $a/R = 1/3$. The Cyclone case, which has been used in many other investigations, is also an obvious choice as a baseline; we choose a slightly higher temperature gradient, however, because we are interested in situations where flow shear stabilisation leads to substantially improved confinement. For this Cyclone-like case, $q = 1.4$, $(r/q)dq/dr = 0.8$, $R/L_T = 8$ at $r/a = 0.5$, and $a/R = 0.36$. Circular concentric model equilibria are used for both simulations. The simulations were run using an adiabatic electron model. In order to limit the flow amplitude at the inner and outer simulation boundaries, while treating a reasonably broad turbulent region, $>100r_\text{i}$, the simulations were run at fairly small $\rho^* = 1/400$, on an annular domain $r \in [0.3, 0.83]$. Noise was controlled using a Krook operator with damping rate $0.008c_\text{i}/a$, as described in Ref. 5, but with toroidal flow conservation also enforced.

First, a set of linear simulations were run for the Cyclone case, with pure poloidal flows, and it was found that a background flow with a shearing rate of $0.05c_\text{i}/a$ is sufficient to almost completely stabilise the system (Fig. 1), although there is a small residual growth rate of $\sim 0.009c_\text{i}/a$. Strong linear suppression with arbitrarily small values of flow shear would be predicted in flux tube simulations, because adding a small flow qualitatively changes the nature of the linear spectrum, in much the same way as adding a small resistivity fundamentally changes the nature of the ideal MHD spectrum. We find a somewhat less dramatic, but still strong, stabilisation in this global analysis. Interestingly, the maximum growth rate in these simulations occurs not for zero flow shear, but for small positive flow shear: the profile shearing which results from the radial variation of the local mode frequency $\omega(r)$ is exactly cancelled by the flow shear at this point. Second, a nonlinear scan of Cyclone cases were run with shearing rates $[0, \pm 0.025, \pm 0.05, \pm 0.10, \pm 0.12, \pm 0.15, \pm 0.2](a/c_\text{s})$. It was necessary to start nonlinear simulations with large initial perturbations, as in Ref. 4, because the cases with large shear are marginally or completely
linearly stable, and the simulations are run over a relatively short timescale of $[0.800]a/c_s$. Substantial heat fluxes are seen for shearing rates several times larger than the point where linear growth rates are almost zero, so that there is a broad region of subcritical turbulence. The non-linear stabilization by the sheared flow, therefore, cannot be directly explained by a reduction in linear growth rates: quasilinear predictions would be expected to be problematic in plasmas with shear flow.

The changes in radially averaged shearing rate during the simulations, which fall in the range $[-0.02, 0.03]\{c_s/a\}$, are much smaller than the range of shearing rates considered, $[-0.2, 0.2]$, so the conclusions on the effects of shearing rate remain the same whether we use the initial or final shearing rates for comparisons. Fig. 1 shows the thermal diffusivities in the simulation versus the shearing rate. Despite some scatter, the dependence of thermal diffusivity on shearing rate can be well modelled by parabolas except for the highest shearing rates where turbulence is suppressed entirely. The turbulence is entirely suppressed when the shearing rate is $|\omega_a| \sim 0.8|\omega_{ITG}|$ or $\sim 1.0|\omega_{ITG}|$ for poloidal and toroidal flows, respectively. Reference 4 also saw evidence of subcriticality for initial shearing rates close to the quench point, where large perturbations were required to achieve sustained turbulence: this phenomenon is more marked in our Cyclone simulations, which required large initial perturbations even for relatively small shearing rates, $\omega_a \geq 0.05c_s/a$. For the simulations with substantial thermal diffusivity and toroidal flows, the flux of parallel momentum $\Gamma_{||}$ is roughly proportional to the product of the radial derivative of the parallel flow profile and the heat flux. The ratio of the effective momentum diffusivity to the heat diffusivity, the Prandtl number, found by linear fitting, is $\sim 0.4$.

We also ran simulations with relatively large shear-free rotation of $0.04c_s$ and $-0.04c_s$ and found a diffusivity of $2.6$ and $2.5|\omega_{ITG}|$, respectively, indicating that diffusivity is largely independent of the flow rate over the range $[-0.04, 0.04]c_s$. The maximum flow rate $v_{E < B}$ in the sheared simulations is $0.04c_s$. We, therefore, do not expect the magnitude of the flow to influence the diffusivity in the inner and outer parts of the sheared simulations.

For the STD case, a scan was conducted for shearing rates over the range $[-0.145, 0.145]c_s/a$ with pure toroidal flows and $[-0.09, 0.09]c_s/a$ with pure poloidal flows. The diffusivities agree relatively well with the adiabatic electron cases in Refs. 4 and 7, for either sign of shearing rate; the local simulations are expected to be insensitive to the sign of the shearing rate for up-down symmetric equilibria, due to a symmetry of the local gyrokinetic equations. Although we do not plot it here, the uncertainty due to turbulent fluctuation is of the order of $20\%$. The range of shearing rates examined here is somewhat smaller than those in Refs. 4 and 7 in order to avoid excessively large flows near the inboard and outboard edge of the annulus: to examine larger shearing rates, we would need to consider a smaller annulus of a larger plasma, nearer the local limit. The Prandtl number is around 0.5 (for the three cases with nonzero velocity shear), in rough agreement with, although the scatter is too large to recover the dependence on shear.

Notably, both poloidal and toroidal shear flow allow complete turbulence stabilisation in the Cyclone case, whereas in the STD case, toroidal shear flow does not substantially suppress turbulence. In the Cyclone case, the toroidal shear flow required to produce a substantial shear on the turbulent structures is considerably lower (due to lower $q$ and $R/a$) and the temperature gradient is relatively close to critical. This may explain why the destabilising effects of parallel shear flow which is introduced when considering toroidal, rather than poloidal, shear flows, is weaker in the Cyclone case.

Figures 2(a) and 2(b) show inward propagating bursts across the simulation domain for positive shearing rates and outwards propagating bursts for positive shearing rates. This can be quantitatively confirmed by considering 2D

\[ \text{FIG. 2. Flux versus time and radius for the Cyclone-like simulations with background shear (a) 0.1a/c_s and (b) } -0.1a/c_s. \]
autocorrelation diagrams, as in Ref. 8; the dominant correlations along the lines $\delta r = v \delta t$, where $v$ is the burst velocity, suggest that most of the time variation in heat flux is associated with bursts. This is consistent with the results and theory presented in Ref. 8. We also observe a shift in the diffusivity profile as a function of shearing rate (Fig. 3), which may be due to a process which we call “turbulence convection” in analogy with the “turbulence spreading” proposed by others: 9 the bursts carry information about turbulence levels across the minor radius, which may modify the steady state fluxes that would be expected in a local picture. Given that bursts can propagate across a large proportion of the turbulent region, simulation results in the centre of the annulus may depend on boundary conditions, because the bursts could be generated at the boundary. This is despite the active region being 150 gyroradii wide, comparable to the radial extents used in typical flux tube calculations, and a sizeable proportion of the width of the core in experiments like JET.

IV. SIMULATIONS CONTAINING ZONE BOUNDARIES

Quasi-steady state turbulently generated flows tend to self-organise into a zig-zag structure, with alternating domains of roughly constant positive and negative poloidal flow shear. To model a plasma containing a boundary between two flow zones, we consider a “V-shaped” flow profile, with two zones of opposite but equal flow shear, and set the interface between the two zones at roughly mid-radius, as shown in Figure 4. Here, we have flow shear profiles of the form

$$\omega(r)_{ESB} = -\omega_0 \text{sign}(r - r_0).$$  \hfill (8)

First, we perform a linear stability analysis of the Cyclone test case with poloidal “V-shaped” flows of varying amplitude, $\omega_0$, and at different values of temperature gradient. In linear simulations with V-shaped flow, the unstable mode is radially localised near the zone boundary; the strong linear stabilisation resulting from homogeneous flow shear appears to be enough to locally damp the mode away from this inhomogeneity. At low values of temperature gradient (Fig. 5), introducing flow shear reduces the growth rate. Note that the stabilisation with flow shear depends strongly on the sign of the “V,” and that positive V-flows are much less effective for stabilisation. For large enough negative V-profiles and larger temperature gradients, the plasma becomes more unstable with increasing shear, so that only a finite “window” in flow shear is stable. At a certain temperature gradient $\nabla T > 6.3$, there is no longer any stable value of $\omega_0$. This should be contrasted with the situation for homogeneous shear flows (see Fig. 1(a)), where a shearing rate of $0.05 c_s/a$ is sufficient to almost completely stabilise the flows at $R/L_T = 8.3$, higher than any considered here.

As a rough method to characterise the interaction of these linear modes with the poloidal flow, we consider the profiles of radial gyrocentre flux $\Gamma$. This gyroflux induces a prompt modification of the axisymmetric radial electric field. The zonal electric field is also influenced by a radial

FIG. 3. (Color online) The mean position of the heat flux profile, $\langle r \Lambda \rangle / \langle \Lambda \rangle$, as a function of shearing rate. A linear fit is show for comparison.

FIG. 4. (Color online) Components of poloidal flow for simulations with an imposed V-shaped poloidal flow (a) and toroidal flow (b) with $\omega_0 = 0.2$. The initial profiles and those at the end of the simulation are shown as thin lines and thick lines, respectively.
shear flow suppression, with V shaped flows, at the coexistence of such states. For a sinusoidal flow profile, to determine the range of existence of the Dimits shift. The temperature gradient where all flow states are unstable (between $-0.12 \alpha$ and $0.2 \alpha$), indicating that there is a saturation mechanism acting to limit the global shear. For these cases, $\omega_{E,B}^2$ stabilises its final value about $300\alpha c_s^2$ into the nonlinear period. Even for $\omega_{E,B}^2 < 0.12 \alpha$, the value of $\omega_{E,B}^2$ decreases somewhat during the simulation, so that for negative V-flows, the absolute shear actually increases. It is well known from previous gyrokinetic simulations that small-scale zonal flow shear to saturate at $\sim 0.2 \alpha / c_s$; this also occurs for positive V-shaped flows on long length scales.

The late time diffusivity is not strongly dependent on the sign of the flow profile, but only the magnitude of the late time $|\omega_{E,B}^2|$. The average late time heat flux both in these simulations and those of Sec. II is well predicted by the late time $|\omega_{E,B}^2|$ (the parabolic fit used in 1 is reproduced in 7 for comparison). However, this is no longer the case when the early time behaviour is considered. The simulations with large initial positive V-flow show large diffusivity in the early stages, $2 - 3 \alpha L_{GB}$, as the flow profile evolves towards saturation, unlike the simulations with large negative V-flows, which show almost complete turbulence suppression. To accurately quantify the diffusivity levels for large positive V-flows, we would need to artificially maintain the global flow profile: nevertheless, we conclude that positive V-flows are less effective for turbulence suppression than negative V-flows.

The complete suppression of late-time turbulence seen at the largest negative $\omega_{\nu}$ is not surprising given the very strong (but not complete) linear stabilisation at $R/L_T = 6.94$. At positive $\omega_{\nu}$, the linear theory suggests only a small suppression of turbulence at the boundary. This is broadly consistent with the high levels of turbulence seen in the nonlinear simulations with large positive $\omega_{\nu}$ at early time. Unlike in the case with homogenous shear flows, the regimes of linear and nonlinear stability coincide moderately well. The much stronger flow profile evolution seen for cases with large positive $\omega_{\nu}$ is also consistent with the large normalised gyrodensity flux in linear modes at large positive $\omega_{\nu}$ (assuming that ratio between heat flux and gyrodensity flux stays roughly constant in the nonlinear regime).

The stronger linear stability and lower diffusivity for negative $\omega_{\nu}$ provide a plausible explanation for the correlation between $E_r$ and the perturbed temperature gradient $\delta(R/L_T)$ seen in earlier ITG simulations. Figure 8 shows the temperature gradient fluctuation and $E_r$ profile averaged over $60\alpha c_s$ in an earlier CYCLONE-type simulation with $\rho^* = 1/280$ and no heat source. We can clearly see that the temperature gradient profile and the $E_r$ profile are correlated on short scales but not exactly proportional: the strong change in temperature gradient at the edge of the turbulent region is not really reflected in $E_r$. Radial profiles of

FIG. 5. (Color online) ITG growth rate versus imposed flow shear amplitude for “V-shaped” flow profile.

FIG. 6. (Color online) Gyrocentre flux versus radius, normalised to maximum heat flux, for V-shaped profiles, with $R/L_T = 6.94$. Redistribution which occurs on the bounce time due to the parallel velocity dependence of the perturbation, which we do not analyse. In Figure 6, we plot $\Gamma$ normalised to the maximum heat flux for the linear eigenmodes of the $R/L_T = 6.94$ case. In each case, the gyrodensity perturbation produced by the flux would act to reduce the flow at the zone boundary. By far, the strongest normalised gyrocentre flux occurs for the case with large positive V-profile.

The fact that there are stable equilibria with flow above the zero-flow stability limit can be considered a manifestation of the Dimits shift. The temperature gradient where all flow states are unstable (between $R/L_T = 6.25$ and 6.94) is roughly equal to the nonlinear critical gradient in Ref. 11. An analogous linear stability analysis was performed in Ref. 12 for a sinusoidal flow profile, to determine the range of existence of such states. A nonlinear scan is then performed to further investigate shear flow suppression, with V shaped flows, at $R/L_T = 8.0$. In these simulations, in contrast to the simulations with homogeneous shear, the overall flow profile undergoes substantial time evolution when the initial V shaped flow is strongly positive: the turbulently generated flows act to reduce the peak flow in this case. To quantify this reduction in global shear, we measure the overall $E \times B$ shear rate in the left ($\omega_l$) and right ($\omega_r$) half of the “V,” and define an large-scale shearing rate $\omega_{\nu}^2 = \omega_l^2 - \omega_r^2$. At the start of the simulation, $|\omega_{E,B}^2|$ is equal to the mean absolute value of the shearing rate. We plot the diffusivity versus initial and final $\omega_{E,B}^2$ in Fig. 7(a). Unlike in the simulations of Sec. II, there is a marked trend for $\omega_{E,B}^2$ to decrease. For large enough initial V-shaped flow, the final $\omega_{E,B}^2$ decreases to roughly 0.12$\alpha c_s^2$, indicating that there is a saturation mechanism acting to limit the global shear. For these cases, $\omega_{E,B}^2$ stabilises its final value about $300\alpha c_s^2$ into the nonlinear period. Even for $\omega_{E,B}^2 < 0.12 \alpha$, the value of $\omega_{E,B}^2$ decreases somewhat during the simulation, so that for negative V-flows, the absolute shear actually increases. It is well known from previous gyrokinetic simulations that small-scale zonal flow shear to saturate at $\sim 0.2 \alpha / c_s$; this also occurs for positive V-shaped flows on long length scales.

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temperature gradient and $E_r$ show corrugations on the zonal flow wavelength, with lower $R/L_T$ at negative zone boundaries, and higher $R/L_T$ at positive zone boundaries; lower temperature gradient compensates for the larger diffusivity in order that the heat flux be radially uniform.

Other authors have suggested that the sum of the diamagnetic and $E/C^2B$ flow is dynamically conserved even in collisionless simulations, or found similar correlations during bursts in weakly collisional simulations and ascribed them to radial force balance. However, it is clear from Figure 8 that the sum of the diamagnetic ($\propto dT/dr$) and $E \times B$ flows is not conserved, and we know of no reason to expect this quantity to be conserved except on the collision timescale.

An important difference between the physics with positive and negative V-shaped flow is the propagation of bursts in the system. Again, the burst direction depends on the local sign of the flow shear, so bursts travel outwards from (inwards towards) the zone boundary for positive (negative) V-flows. Dynamics at the positive V-boundary might, therefore, be expected to have a strong nonlocal effect on the plasma.

When V-shaped toroidal flows are specified, the overall dynamics are similar to the simulations with V-shaped poloidal flows. The $E_r$ profile evolution is similar, as is the thermal transport level. We were able to perform a wider scan in initial shearing rate with pure toroidal flows than poloidal flows, because the restriction that the toroidal flow be a small fraction of the sound speed is less strict than the requirement for poloidal flows not to excessively distort the background distribution. One complication that arises when V-shaped toroidal flows are added is that the reconstructed temperature gradient profile becomes somewhat sensitive to the input parameter $\alpha_v$, with a bump or hole appearing at the reversal point (this effect is proportional to $q^3$). For these simulations, we turn off the heat source inside the turbulent region [0.4, 0.7], to allow the temperature profile to relax to a self-consistent steady state: the localised inhomogeneity in the temperature profile is rapidly removed, well before substantial changes to the flow profile occur. A side-effect is that the temperature gradient profiles are less well controlled, so that the simulations with larger diffusivities tend to have lower local temperature gradients.

For pure toroidal flows (Fig. 7(b)), the transport does almost completely stabilise for sufficiently strong positive V-flows, at about 1.5 times the level needed for negative V-flows. Another important feature is that the dynamics of $E \times B$ and parallel flows are qualitatively quite different. The $E \times B$ flow evolution is similar to that in the pure poloidal flow cases, so that for large positive V-flow, $\omega_{E\times B}$ decreases to the saturation level, but otherwise remains roughly constant. The toroidal flow evolution, on the other hand, looks like a simple diffusion process dependent on the turbulence

![Figure 7](image1.png)

**FIG. 7.** (Color online) Diffusivity versus large-scale shearing rate, $\omega_{ExB}$, for simulations with an imposed V-shaped poloidal flow (a) and toroidal flow (b). Diamonds show initial $\omega_{ExB}$ and squares show $\omega_{ExB}$ averaged over the last half of the simulation. The parabola is the fit from 1, where a homogeneous flow was imposed.

![Figure 8](image2.png)

**FIG. 8.** (Color online) Profiles of temperature gradient fluctuations (thin line) and the radial derivative of the zonal potential (thick line) versus radius, averaged over the last 60$a/c_s$ of an ITG simulation without a heat source.
level, with the originally V-shaped parallel flow profile itself evolving to a smooth hump in cases where there is a substantial turbulence level (Figure 4(b) is typical).

It would be difficult to explain these global flow dynamics using a 1D transport equation, where poloidal and toroidal flow dynamics are determined via momentum fluxes dependent on the local gradients. For pure poloidal flows, there is little global flow reorganisation in the system with homogeneous shear flows. If we used the homogeneous shear simulations as a basis for a model of flow dynamics, we would also expect to see little poloidal flow evolution in the simulations with V-shaped flows, but we do see a strong flow reorganisation. In both pure toroidal and pure poloidal flow simulations, the effective (toroidal or poloidal) momentum diffusivity is strongly dependent on the sign of the flow profile, which is surprising, because flux-tube models of up-down symmetric equilibria are symmetric with respect to the sign of the shearing rate.

V. DISCUSSION AND CONCLUSIONS

We have modelled the effects of two different forms of flow profiles on turbulence levels and examined the time evolution of the flow profile. For homogeneous flow shear profiles, both toroidal and poloidal flow can completely suppress turbulence for some parameter choices, well above the Dimits shift region. Little $E \times B$ flow profile evolution is seen on the timescale of the simulation for homogeneous flows. On the other hand, for the non-homogeneous flow profiles, the $E \times B$ component of positive V-shaped flow profiles can rapidly decay to a saturated state.

The results help to explain why small-scale zonal flows and large scale homogeneous shear flows have different impacts on turbulence. Inhomogeneities, and, in particular, zonal flow boundaries, play a crucial role and can modify the turbulent dynamics over a substantial region. For the V shaped profiles, dynamics over a simulation domain $\sim 150$ gyroradii wide is critically modified when a flow shear boundary is introduced. The zone boundaries appear to control poloidal flow reorganisation in these systems and induce the saturation in $E \times B$ shear flow level seen in typical ITG simulations. The poloidal flow does not saturate in simulations with homogeneous imposed fields, where no zone boundaries are present.

In addition, the thermal and toroidal momentum fluxes depend not only on the magnitude of the local $E \times B$ shearing rate, but on the overall flow profile over a wide region. The presence of strong nonlocal effects is correlated with the presence of bursts which can traverse a wide radial extent in strongly sheared plasmas.

This allows some insight into the effects of more general flow profiles which would be relevant to experiments, which are not generally homogeneous. For example, flow profiles associated with transport barriers have relatively short wavelength features. Models of transport barriers using homogeneous shear flows might predict stabilisation for strong enough shear, but the saturation effect shown here may limit the shearing rate and prevent turbulence suppression.

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