

First Measurement of the Damping Rate of High-n Toroidal Alfvén Eigenmodes in JET Tokamak Plasmas

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*See the Appendix of M.L. Watkins et al., Fusion Energy 2006 (Proc. 21st Int. Conf. Chengdu, 2006), IAEA.

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INTRODUCTION

After many years of successful operation, the JET saddle coil system was dismantled during the 2004-2005 shutdown [1]. A new antenna system was installed to replace it and excite MHD modes in the Alfvén frequency range, with similar operational capabilities [2].

Why Study Alfvén Waves?

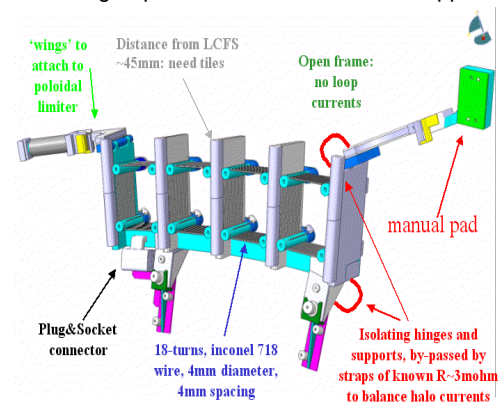
Why Replace the Saddle Coils?

1. fusion-born alpha particles (α 's) resonate with Alfvén Waves (AWs) if $\omega = k_{||} v_A$
2. AW spectrum unstable if large-enough free energy in the fast ion pressure gradient
3. an unstable AW spectrum can lead to direct α 's losses, possibly quenching the ignition process and damaging the first wall due to their geometry, the saddle coils only drive low toroidal mode numbers, $|n| < 2$
4. ITER predictions [3]: most unstable modes have $n \sim 5-20$ (already observed in JET)

→ therefore difficult to extrapolate directly low-n results to burning plasmas and ITER

ANTENNA DESIGN PRINCIPLES AND OPERATIONAL RESULTS

- total halo current integrated over the antenna surface = 90kA ($I_{p0}=6\text{MA}$, $I_{\text{HALO}}/I_{p0}=30\%$, $\text{TPF}=1.4$)
- loop voltage at disruptions: 800V/6MA, $\sim 25\text{V}$ at each bellow (avoid close toroidal path of low R)
- radiative power up to 150kW/m² for >30sec; energy blip at disruptions $\sim 1\text{MJ/m}^2$ over <1ms
- antennas mounted on an open frame, to avoid a closed path for disruption-induced currents
- frame attached to poloidal limiter via 3m Ω resistive straps to optimise the load distribution
- antennas and frame protected by CFC tiles mounted on private mini-limiters
- small compact antennas: 18 turns, NA $\sim 1\text{m}^2$ (saddle coils: NA $\sim 15\text{m}^2$)
- antenna-plasma distance: 60mm to LCFS (saddle coils: 20mm to LCFS)
- two groups of four antennas each at opposite toroidal locations to control driven n-spectrum



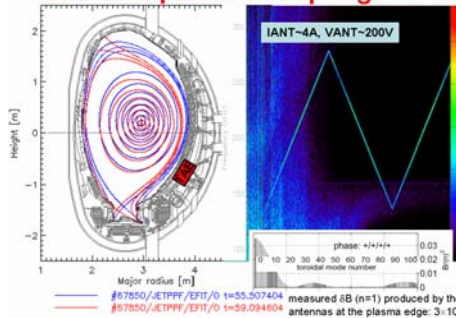
Close-up showing various engineering details.



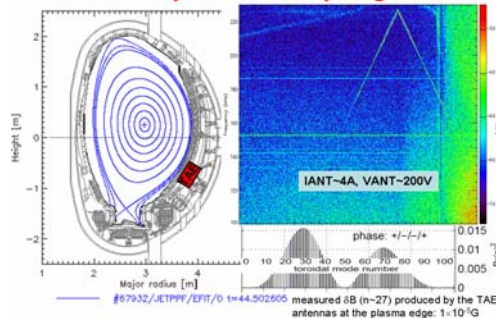
AE antennas as installed in-vessel in June 2005.

- excited n-spectrum: easily up to $n \sim 30$ for different antenna phasing configurations

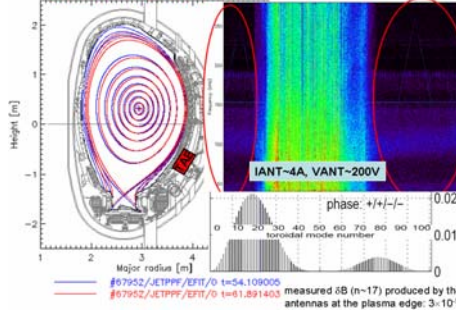
antenna-plasma coupling: ++++



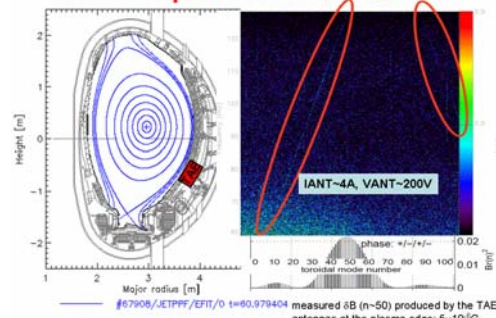
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antenna-plasma coupling: ++--



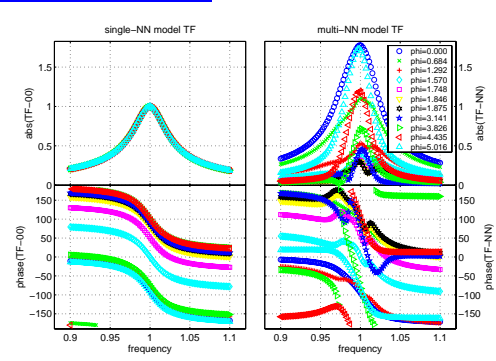
antenna-plasma coupling: +-+-



Calculated (vacuum) excitation spectra obtained using different antenna phasing configurations.

PROBLEMATIC DETERMINATION OF TOROIDAL MODE NUMBERS

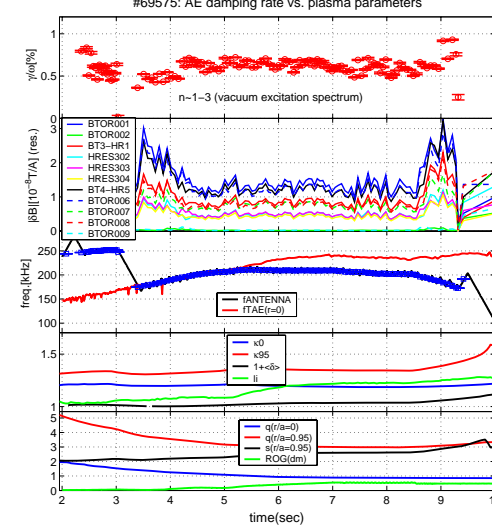
- saddle coils: almost pure $n=1/n=2$ spectrum, other harmonics <10% in power spectrum
- new antennas: (vacuum) excited spectrum is multi-harmonics, with typical HFWM>10
- limited number of pick-up coils, no reliable internal measurements of AE mode structure
- hence very difficult to separate precisely the different harmonics and evaluate the frequency and damping rate for each one
- comparison (see figure): predicted TAE signal at each pick-up coil for one mode ($n=5$, $\omega_n=1$, $\gamma_n=2\%$) and five modes ($n=3-7$, closely spaced in frequency: $\Delta\omega_n=2\%$, $\gamma_n[\%]=0.2-1.0$)



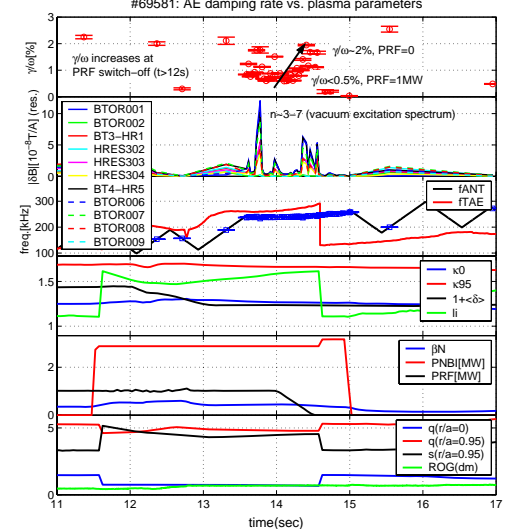
- most promising method so far: combine vacuum excitation spectrum with results from "SparSpec" code [4] (previously used for the analysis of astrophysical data)

FIRST QUALITATIVE EXPERIMENTAL RESULTS

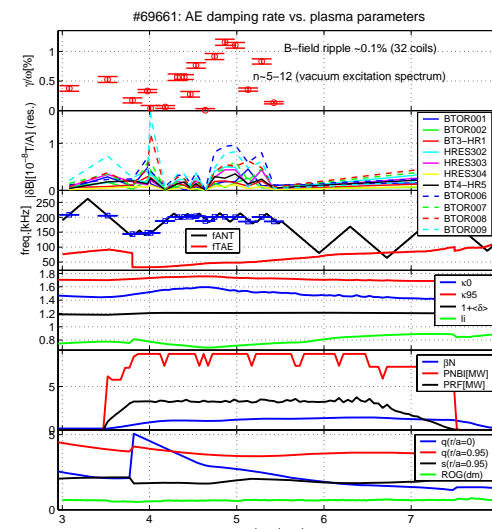
- n-number spectrum tentatively inferred from the vacuum antenna excitation spectrum
- qualitative measurements of the damping rate to be considered as an upper limit to the value for each individual n-component
- benchmark against saddle coils data: measured γ/ω for low-n TAEs in ohmic plasmas with low edge elongation is the same → essential verification!



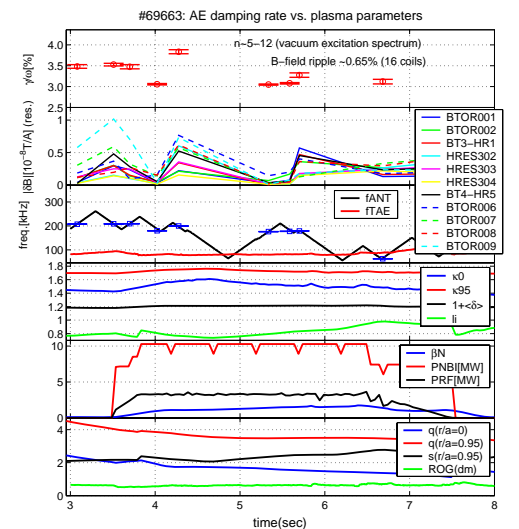
For ohmic plasmas with low edge elongation, the damping rate of low-n ($n \sim 1-3$) TAEs, as measured with the new AE antennas, is identical to that measured with the old saddle coils



At the ICRF power switch-off, the damping rate γ/ω of $n \sim 3-7$ TAEs increases linearly with P_{ICRF} for otherwise constant plasma parameters (NBI power, edge elongation and magnetic shear).



when the fast ion drive is provided by resonant NBI ions with $v_{||\text{NBI}} \sim v_A/3$, the damping rate of $n \sim 5-15$ TAEs increases to $\gamma/\omega \sim 3\%$ in the presence of a $\sim 0.65\%$ B-field ripple, compared to $\gamma/\omega \sim 1\%$ without B-field ripple. These data provide examples of a direct estimate of the fast ion drive to these modes.



CONCLUSIONS

- first measurement of the damping rate of AEs with $n \sim 1-30$ with new antennas in JET
- routine real-time mode detection and tracking even with small antennas located far away from LCFS → possible use in ITER for burn control applications?
- problematic determination of n's because of complex excitation spectrum
- various numerical tools being assessed and developed for accurate n-spectrum separation

OUTLOOK AND FUTURE WORK

- second set of new antennas to be installed during the forthcoming shutdown: simultaneous use of the two sets (located at toroidally symmetric positions) is expected to provide a narrower antenna excitation spectrum, hence possibly simplify the damping rate analysis
- internal measurements of the AE mode structure may become more reliable, hence providing insights for determining the antenna-driven mode structure
- testing of the different analysis methods to de-convolve the driven multi-n antenna spectrum is expected to be completed, so that more quantitative measurements of the mode frequency and damping rate for individual toroidal mode numbers will become available
- comparison with previous results for medium-n TAEs from Alcator C-mod [5]

ACKNOWLEDGEMENT

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 [5] J. Snipes et al, Plasma Phys. Control. Fusion **46** (2004), 611.